

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization International Bureau



(43) International Publication Date
14 April 2005 (14.04.2005)

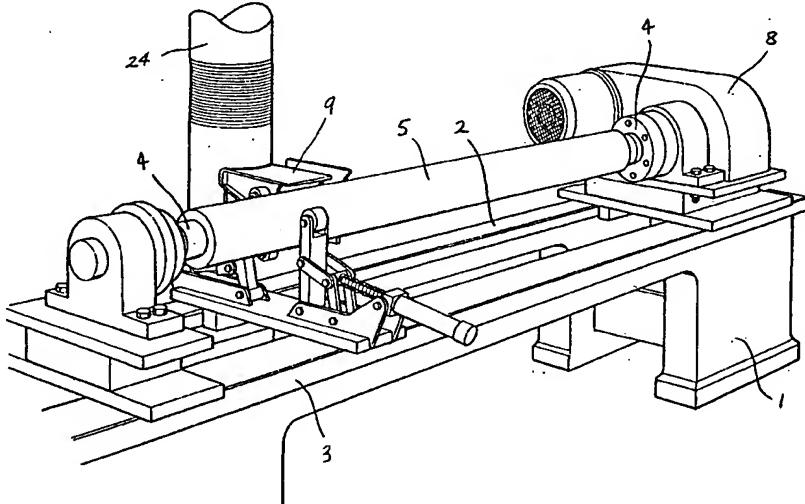
PCT

(10) International Publication Number
WO 2005/032784 A1

- (51) International Patent Classification⁷: B28B 21/92,
21/96, E04C 3/34
- (21) International Application Number:
PCT/AU2004/001378
- (22) International Filing Date: 8 October 2004 (08.10.2004)
- (25) Filing Language: English
- (26) Publication Language: English
- (30) Priority Data:
2003905479 8 October 2003 (08.10.2003) AU
- (71) Applicant (*for all designated States except US*): JAMES HARDIE INTERNATIONAL FINANCE B.V. [NL/NL]; Unit 04-07, Atrium Building, Strawinskylaan 3077, NL-1077ZX Amsterdam (NL).
- (72) Inventors; and
- (75) Inventors/Applicants (*for US only*): GLEESON, James [AU/AU]; 11 Blckwood Road, North Curl Curl, NSW 2099 (AU). GIBSON, Kevin [AU/UA]; 4 Jessie Court, Albany Creek, QLD 4035 (AU). PORFLIDA, Michael [AU/AU]; 6 Ostend Street, Lidcombe, NSW 2141 (AU). HOGAN, Michael [AU/AU]; James Hardie Research Pty Limited, Level 1, Research & Product Development Bulding, 10 Colquhoun Street, Rosehill, NSW 2142 (AU).
- (74) Agent: SHELSTON IP; 60 Margaret Street, Sydney NSW 2000 (AU).
- (81) Designated States (*unless otherwise indicated, for every kind of national protection available*): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NA, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.
- (84) Designated States (*unless otherwise indicated, for every kind of regional protection available*): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PL, PT, RO, SE, SI,

{Continued on next page}

(54) Title: A FIBRE REINFORCED CEMENT COLUMN AND METHOD OF FORMING THE SAME



WO 2005/032784 A1

(57) Abstract: A fibre reinforced cement (FRC) tubular body having a wall thickness to outer diameter ratio of less than around 0.050, preferably 0.035. A lathe assembly and method for forming an elongate tubular body, such as said FRC tubular body, is also claimed, said lathe assembly including: an elongate base (1); a pair of chucks (4) located at opposite longitudinal ends of said base (1), said chucks (4) being configured to engage opposite longitudinal ends of the tubular body; two or more lateral supports (11, 12, 17) connected to said base to support the tubular body at two or more support locations between its ends; drive means (8) for rotating the body about a longitudinal axis; and a profiling tool (9) connected to the base and engageable to machine or profile an outer circumferential surface of the tubular body.



SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ,
GW, ML, MR, NE, SN, TD, TG).

Declaration under Rule 4.17:
— of inventorship (Rule 4.17(iv)) for US only

Published:

— with international search report

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

- 1 -

"A FIBRE REINFORCED CEMENT COLUMN AND METHOD OF FORMING THE SAME"

This invention relates to the design and manufacture of tubular bodies such as columns or pipes. The invention has been developed primarily in relation to 5 architectural columns manufactured from Fibre Reinforced Cement (FRC) and will be described hereinafter with reference to this application. However, it will be appreciated that the invention is not limited to this particular material or field of use.

BACKGROUND OF THE INVENTION

The following discussion of the prior art is intended to place the invention in an 10 appropriate technical context and to allow its significance to be properly appreciated. However, any references to the prior art should not be construed as admissions that such prior art is widely known or forms part of common general knowledge in the field.

Known methods of machining tubular columns have typically involved mounting 15 the column on a lathe using a rotatable chuck at each end of the column. Once engaged by the chucks, a single support roller is brought into contact with the outer surface of the column to provide lateral support for the column during the machining process.

The outer circumference of the column is then machined to the desired profile using a machining head located opposite the support roller. Typically both the support 20 roller and the machining head are mounted on a rail or slide extending along the length of the lathe. In this way, the machining head and the support roller can be driven progressively along the length of the column, machining the column as they move, and without moving out of relative alignment with one another.

This known method of forming tubular columns tends to work reasonably well 25 with columns having relatively thick walls. However, the applicant has found that if thinner walled columns are profiled using the prior art method, the columns tend to vibrate excessively when rotated on the lathe, resulting in fracture or severe surface grooving of the columns during the machining process. This problem is particularly pertinent in the context of FRC columns and pipes. Consequently, such columns are required to be formed with wall thicknesses greater than the intended application would

- 2 -

dictate in structural terms, which increases the requirement for raw materials, cost and weight, while compromising handlability.

It is an object of the present invention to overcome or ameliorate one or more of the disadvantages of the prior art, or at least to provide a useful alternative.

5 DISCLOSURE OF THE INVENTION

A first aspect of the invention provides a Fibre Reinforced Cement tubular body having a wall thickness to outer diameter ratio of less than around 0.050.

Preferably, the body has a wall thickness to outer diameter ratio of less than around 0.045. More preferably, the body has a wall thickness to outer diameter ratio of 10 less than around 0.035.

Preferably, an outer circumferential surface of the body is machined or profiled until the wall thickness to outer diameter ratio defined above is achieved.

More preferably, the body is profiled using a method including the steps of:
15 supporting the body at or adjacent its ends for rotation about a longitudinal axis;
supporting the body laterally at two or more lateral support locations between the ends;
rotating the body about the longitudinal axis; and
machining or profiling an outer surface of the body using a profiling tool.

Preferably, the tubular body is designed for use as an architectural column, but 20 may alternatively be intended for use as a pipe, structural member, a concrete forming element or for some other purpose.

Preferably, the two or more lateral support locations are disposed at substantially the same position along the length of the column. More preferably, the two or more lateral support locations are spaced circumferentially around the column.

25 Alternatively, the two or more support locations may be located at different axial positions along the column. In this alternative embodiment, the support locations are preferably also spaced circumferentially around the column.

- 3 -

Preferably, the lateral support is provided by respective support rollers engageable with an outer circumferential surface of the column. The support rollers and the profiling tool are preferably adapted to move in unison along the length of the column during the profiling operation. Preferably, two of the support rollers are independently movable into engagement with the column. More preferably, three support rollers are provided, two of the support rollers being movable into engagement with the column independently of the third support roller. Even more preferably, two of the support rollers are dependently movable into engagement with the column.

Preferably, the dependently movable support rollers are hingedly mounted to opposite ends of a first bell crank having an axis of rotation substantially parallel to the longitudinal axis of the column. More preferably, the first bell crank is hingedly connected to one end of a second bell crank having an axis of rotation parallel to the longitudinal axis of the column.

Preferably, the other end of the second bell crank is rotatably connected to a first base plate. More preferably, the first base plate is longitudinally movable along the elongate base. Even more preferably, the first base plate is selectively fixedly connectable to the elongate base in any one of a plurality of axial locations. Preferably, the independently movable support roller is mounted to one end of a pivotal arm. More preferably, the arm has an axis of rotation parallel to the longitudinal axis of the column.

Preferably, the other end of the arm is hingedly connected to a second base plate. More preferably, the second base plate is longitudinally movable along the elongate base. Even more preferably, the second base plate is selectively fixably connectable to the elongate base in any one of a plurality of axial locations.

Preferably, the method includes the additional step of progressively moving the first and second base plates and the profiling tool simultaneously along the column during the profiling step.

Preferably, at least one of the support rollers is configured to move axially in response to imperfections in the outer circumferential surface of the column.

Preferably, the profiling tool when in use is located axially adjacent one of the lateral support locations.

Preferably, the FRC column to be profiled is a blank formed on a mandrel using a Hatschek process. The machining or profiling step is preferably used to substantially reduce the initial wall thickness and refine the surface finish of the blank to form the architectural column.

5 Preferably, the column has a wall thickness to outer diameter ratio of less than around 0.050. More preferably, the column has a wall thickness to outer diameter ratio of less than around 0.045. Even more preferably, the column has a wall thickness to outer diameter ratio of less than around 0.035.

10 Preferably, the column is profiled on a lathe assembly including:
an elongate base;
a pair of chucks located at opposite longitudinal ends of said base, said chucks being configured to engage opposite longitudinal ends of the column;
two or more lateral supports connected to said base to support the column at two or more support locations between its ends;
15 drive means for rotating the column about a longitudinal axis; and
a profiling tool connected to the base and engageable to machine or profile an outer circumferential surface of the column.

20 Preferably, the two or more lateral supports are located at substantially the same axial position along the length of the column relative to one another. More preferably, the supports are spaced circumferentially around the column.

Alternatively, the two or more supports are located at different points along the length of the column. More preferably, in this alternative embodiment, the support locations are also spaced circumferentially around the column.

25 Preferably, the lateral supports take the form of support rollers engageable with an outer circumferential surface of the column. Preferably, two of the support rollers are independently movable into engagement with the column. More preferably, three support rollers are provided, two of the support rollers being movable into engagement with the column independently of the third support roller. Even more preferably, two of the support rollers are dependently movable into engagement with the column.

- 5 -

5 Preferably, the dependently movable support rollers are hingedly mounted to opposite ends of a first bell crank lever having an axis of rotation substantially parallel to the longitudinal axis of the column. More preferably, the first lever is hingedly connected to one end of a second bell crank lever having an axis of rotation parallel to the longitudinal axis of the column.

10 Preferably, the other end of the second lever is rotatably connected to a first base plate. More preferably, the first base plate is longitudinally movable along the elongate base. Even more preferably, the first base plate is selectively fixably connectable to the elongate base in any one of a plurality of axial locations. Preferably, a pneumatic actuator is operable on the second lever to move the respective rollers into and out of engagement with the column.

15 Preferably, the independently movable support roller is mounted to one end of a pivotal arm. More preferably, the arm has an axis of rotation parallel to the longitudinal axis of the column.

20 15 Preferably, the other end of the arm is hingedly connected to a second base plate. More preferably, the second base plate is longitudinally movable along the elongate base. Even more preferably, the second base plate is selectively fixably connectable to the elongate base in any one of a plurality of axial locations.

25 20 Preferably, a pneumatic actuator is operable on the arm to move the respective roller into and out of engagement with the column.

Preferably, at least one of the support rollers is configured to move radially in response to imperfections in the outer circumferential surface of the column.

25 Preferably, the profiling tool when in use is located axially adjacent one of the support locations. More preferably, the profiling tool is longitudinally movable along the elongate base. Even more preferably, the profiling tool is selectively fixably connectable to the elongate base in any one of a plurality of axial locations.

In a preferred form, the profiling tool, first base plate and second base plate are interconnected such that they move substantially in unison along the rails, so as to remain in relative lateral alignment during profiling operation.

- 6 -

A second aspect of the invention provides a method of manufacturing an elongate tubular body, said method including the steps of:

- supporting the body at or adjacent its ends for rotation about a longitudinal axis;
- supporting the body laterally at two or more lateral support locations between the ends;
- rotating the body about the longitudinal axis; and
- machining or profiling an outer surface of the body using a profiling tool.

Preferably, the tubular body is designed for use as an architectural column, but may alternatively be intended for use as a pipe, structural member, a concrete forming element or for some other purpose.

Preferably, the two or more lateral support locations are disposed at substantially the same position along the length of the column. More preferably, the two or more lateral support locations are spaced circumferentially around the column.

Alternatively, the two or more support locations may be located at different axial positions along the column. In this alternative embodiment, the support locations are preferably also spaced circumferentially around the column.

Preferably, the lateral support is provided by respective support rollers engageable with an outer circumferential surface of the column. The support rollers and the profiling tool are preferably adapted to move in unison along the length of the column during the profiling operation. Preferably, two of the support rollers are independently movable into engagement with the column. More preferably, three support rollers are provided, two of the support rollers being movable into engagement with the column independently of the third support roller. Even more preferably, two of the support rollers are dependently movable into engagement with the column.

Preferably, the dependently movable support rollers are hingedly mounted to opposite ends of a first bell crank having an axis of rotation substantially parallel to the longitudinal axis of the column. More preferably, the first bell crank is hingedly connected to one end of a second bell crank having an axis of rotation parallel to the longitudinal axis of the column.

- 7 -

Preferably, the other end of the second bell crank is rotatably connected to a first base plate. More preferably, the first base plate is longitudinally movable along the elongate base. Even more preferably, the first base plate is selectively fixedly connectable to the elongate base in any one of a plurality of axial locations. Preferably, 5 the independently movable support roller is mounted to one end of a pivotal arm. More preferably, the arm has an axis of rotation parallel to the longitudinal axis of the column.

Preferably, the other end of the arm is hingedly connected to a second base plate. More preferably, the second base plate is longitudinally movable along the elongate base. Even more preferably, the second base plate is selectively fixably connectable to 10 the elongate base in any one of a plurality of axial locations.

Preferably, the method includes the additional step of progressively moving the first and second base plates and the profiling tool simultaneously along the column during the profiling step.

Preferably, at least one of the support rollers is configured to move axially in 15 response to imperfections in the outer circumferential surface of the column.

Preferably, the profiling tool when in use is located axially adjacent one of the lateral support locations.

Preferably, the column is formed of Fibre Reinforced Cement (FRC). Preferably, 20 the FRC column to be profiled is a blank formed on a mandrel using a Hatschek process. The machining or profiling step is preferably used to substantially reduce the initial wall thickness and refine the surface finish of the blank to form the architectural column.

Preferably, the column has a wall thickness to outer diameter ratio of less than around 0.050. More preferably, the column has a wall thickness to outer diameter ratio of less than around 0.045. Even more preferably, the column has a wall thickness to 25 outer diameter ratio of less than around 0.035.

According to a third aspect, the invention provides a lathe assembly for forming an elongate tubular body, said lathe assembly including:
an elongate base;
a pair of chucks located at opposite longitudinal ends of said base, said chucks
30 being configured to engage opposite longitudinal ends of the tubular body;

two or more lateral supports connected to said base to support the tubular body at two or more support locations between its ends;
drive means for rotating the body about a longitudinal axis; and
a profiling tool connected to the base and engageable to machine or profile an outer circumferential surface of the tubular body.

5 Preferably, the tubular body is an architectural column, but may alternatively be intended for use as a pipe, a structural member, a concrete forming element or for some other purpose.

10 Preferably, the two or more lateral supports are located at substantially the same axial position along the length of the column relative to one another. More preferably, the supports are spaced circumferentially around the column.

Alternatively, the two or more supports are located at different points along the length of the column. More preferably, in this alternative embodiment, the support locations are also spaced circumferentially around the column.

15 Preferably, the lateral supports take the form of support rollers engageable with an outer circumferential surface of the column. Preferably, two of the support rollers are independently movable into engagement with the column. More preferably, three support rollers are provided, two of the support rollers being movable into engagement with the column independently of the third support roller. Even more preferably, two of 20 the support rollers are dependently movable into engagement with the column.

25 Preferably, the dependently movable support rollers are hingedly mounted to opposite ends of a first bell crank lever having an axis of rotation substantially parallel to the longitudinal axis of the column. More preferably, the first lever is hingedly connected to one end of a second bell crank lever having an axis of rotation parallel to the longitudinal axis of the column.

Preferably, the other end of the second lever is rotatably connected to a first base plate. More preferably, the first base plate is longitudinally movable along the elongate base. Even more preferably, the first base plate is selectively fixedly connectable to the elongate base in any one of a plurality of axial locations. Preferably, a pneumatic

- 9 -

actuator is operable on the second lever to move the respective rollers into and out of engagement with the column.

Preferably, the independently movable support roller is mounted to one end of a pivotal arm. More preferably, the arm has an axis of rotation parallel to the longitudinal axis of the column.

5. Preferably, the other end of the arm is hingedly connected to a second base plate. More preferably, the second base plate is longitudinally movable along the elongate base. Even more preferably, the second base plate is selectively fixably connectable to the elongate base in any one of a plurality of axial locations.

10. Preferably, a pneumatic actuator is operable on the arm to move the respective roller into and out of engagement with the column.

Preferably, at least one of the support rollers is configured to move radially in response to imperfections in the outer circumferential surface of the column.

15. Preferably, the profiling tool when in use is located axially adjacent one of the support locations. More preferably, the profiling tool is longitudinally movable along the elongate base. Even more preferably, the profiling tool is selectively fixedly connectable to the elongate base in any one of a plurality of axial locations.

In a preferred form, the profiling tool, first base plate and second base plate are interconnected such that they move substantially in unison along the rails, so as to remain in relative lateral alignment during profiling operation.

20. Preferably, the column is formed of Fibre Reinforced Cement.

BRIEF DESCRIPTION OF THE DRAWINGS

A preferred embodiment of the invention will now be described, by way of example only, with reference to the accompanying drawings in which:

25. Figure 1 is a perspective view of a lathe assembly according to one aspect of the invention, shown in use;

Figure 2 is a side elevation of the lathe assembly of Figure 1;

- 10 -

Figure 3 is a cross-sectional view of the lathe assembly of taken on line 3-3 Figure 2;

Figure 4 is a schematic view of a "Classic" shaped column formed on the profiling assembly of Figure 1;

5 Figure 5 is a schematic view of a "Tapered" shaped column formed on the profiling assembly of Figure 1;

Figure 6 is a schematic sectional side elevation of an unfilled load bearing column;

Figure 7 is a sectional plan view taken along line 7-7 of Figure 6

10 Figure 8 is a schematic sectional side elevation of a filled load bearing column in a pinned base arrangement;

Figure 9 is a schematic sectional side elevation of a filled load bearing column in a fixed base arrangement

Figure 10 is a plan view of an unfilled load bearing column with a handrail; and

Figure 11 is a side elevation of the column of Figure 10.

15 **PREFERRED EMBODIMENTS OF THE INVENTION**

Referring to the drawings, the lathe assembly includes an elongate base 1 incorporating a pair of longitudinally extending rails 2 and 3. Chucks 4 are located respectively at opposite ends of the base. The chucks are longitudinally movable with respect to the base and are configured to engage opposite longitudinal ends of a Fibre Reinforced Cement (FRC) column blank 5, to be profiled. Each chuck is selectively fixably connectable to the base in any one of a plurality of axial locations. As best seen in Figure 3, two lateral supports in the form of first 6 and second 7 lathe steadies are connected to the base to support the column blank 5 at respective support locations between the chucks 4. Drive means for rotating the column blank about its longitudinal axis are also provided. In the illustrated embodiment, the drive means take the form of a motor and associated gearbox, within housing 8, and disposed to drive the chucks 4 via a suitable arrangement of belts and pulleys. A profiling assembly 9 is connected to the

- 11 -

base. This assembly includes a profiling head 10 engageable with an outer circumferential surface of the column blank 5.

The first lathe steady 6 includes two support rollers 11 and 12 having respective axes of rotation parallel to the longitudinal axis of the column blank. The rollers are thereby engageable with the outer circumferential surface of the column blank to provide lateral support for the blank during rotation on the lathe. The support rollers are rotatably mounted to opposite ends of a first bell crank lever 13. The lever 13 has an axis of rotation which is movable but which remains parallel to the longitudinal axis of the column blank throughout its locus of movement. The lever 13 is curved in order that its axis of rotation is offset from the axes of rotation of the associated support rollers 11 and 12. The lever 13 in turn is hingedly connected to a second bell crank lever 14. The lever 14 also has an axis of rotation parallel to the longitudinal axis of the blank. The lever 14 is rotatably connected to a first base plate 15. The first base plate is connected to an engaging formation 16 for retaining the first lathe steady on the rail 2. In this way, the first lathe steady is longitudinally movable along the rail 2.

The second lathe steady 7 includes a single support roller 17 having an axis of rotation parallel to the longitudinal axis of the column blank. The roller 17 is engageable with the outer circumferential surface of the column blank to provide lateral support for the blank during rotation on the lathe, in the diametrically opposing position from the lateral support provided by the first lathe steady. The roller 17 is rotatably mounted on a pivotal arm 18. The arm has a pivot axis parallel to the longitudinal axis of the column blank. The arm in turn is pivotably connected to a second base plate 19. The second base plate is connected to an engaging formation 20 for retaining the second lathe steady on the respective longitudinal rail 3. The second lathe steady is thereby longitudinally slidable along the rail 3. The second lathe steady is fixedly connected to the first lathe steady by a cross-member 21.

A first pneumatic actuator 22 is operable on the second bell crank lever 14 of the first lathe steady to move the respective rollers 11 and 12 into and out of engagement with the column blank. A second pneumatic actuator 23 is operable on the pivotal arm 18 of the second lathe steady to move the respective roller 17 into and out of engagement with the column blank.

- 12 -

In the illustrated embodiment, the support rollers 11 and 12 of the first lathe steady are configured to move generally radially in response to imperfections in the outer circumferential surface of the column blank, thereby to absorb vibration and to provide a smoother finish to the blank. The radial movement of the rollers 11 and 12 is facilitated by the bell-crank configuration of the frame 13. The rotational mounting of the frame also serves to ensure equal distribution of forces between the rollers and the column surface, as any slight misalignment of the rollers is automatically corrected by rotation of the frame.

The profiling assembly 9 is connected to the cross-member 21 adjacent the first lathe steady. The profiling assembly is longitudinally movable along the rail 2. The lathe steadies 6 and 7 and the profiling assembly 9 are driven simultaneously along the rails by a motor and associated gearbox (not shown) located between the rails. A vacuum extractor 24 is connected to the profiling assembly to remove dust and waste material machined from the column blank during the profiling operation.

In use, a FRC column blank 5 to be profiled is supported in the lathe assembly by moving the chucks 4 longitudinally into engagement with opposite longitudinal ends of the column. The lathe steadies 6 and 7 are then brought into laterally supporting contact with the column blank 5 by actuating the respective pneumatic actuators, which in turn move the respective support rollers into diametrically opposing engagement with the outer surface of the column blank. The motor and drive assembly are then activated to rotate the chucks and thereby the blank 5. Next, the profiling head 10 on the profiling assembly is brought into profiling engagement with the outer surface of the column blank 5.

During the profiling operation, the lathe steadies 6 and 7 and the profiling assembly 9 are driven progressively in unison along the rails 2 and 3 by the motor located between the rails (not shown), to profile the outer surface of the blank 5 along all or most of its length. However, it will be appreciated that in alternative embodiments the lathe steadies 2 and 3 and profiling assembly 9 may be held stationary and the blank 5 may be moved longitudinally by traversing the chucks 4 along the tracks.

The column blank 5 is typically made from a fibre reinforced cement composition that falls generally within the ranges set out in the table below.

Dry Ingredients	Acceptable range (% by dry weight)
Cement	15 – 50%
Siliceous material	25 – 80%
Fibrous material	0 – 20%
Additives	0 – 40%

Throughout this specification, unless indicated otherwise where there is reference to wt%, all values are with respect to a cement formulation on a dry materials weight basis prior to addition of water and processing.

5 Preferably, the siliceous material in the formulation is ground sand, also known as silica, or fine quartz. Preferably the siliceous material has an average particle size of 1-50 microns, and more preferably 20-30 microns.

10 The fibrous materials used in the formulation can include cellulose such as softwood and hardwood cellulose fibres, non wood cellulose fibres, asbestos, mineral wool, steel fibre, synthetic polymers such as polyamides, polyesters, polypropylene, polyacrylonitrile, polyacrylamide, polymethylpentene, viscose, nylon, PVC, PVA, rayon, glass, ceramic or carbon. Cellulose fibres produced by the Kraft process are preferred.

15 The other additives used in the formulation can be fillers such as mineral oxides, hydroxides and clays, metal oxides and hydroxides, fire retardants such as magnesite, thickeners, silica fume or amorphous silica, colorants, pigments, water sealing agents, water reducing agents, setting rate modifiers, hardeners, filtering aids, plasticisers, dispersants, foaming agents or flocculating agents, water-proofing agents, density modifiers or other processing aids.

20 The thin walled columns produced on the profiling assembly typically have a post-profiling wall thickness to diameter ratio of less than around 0.050. Thicker walled columns made using prior art methods typically have a wall thickness to diameter ratio of greater than 0.050. As will be appreciated by those skilled in the art, the wall thickness to diameter ratio in columns of this type necessarily varies depending on the outer diameter of the column.

- 14 -

The use of the illustrated profiling assembly allows column wall thicknesses to be reduced by around 5mm compared with columns produced using prior art methods. It will be appreciated that this reduction in material results in more lightweight columns. Moreover, it is emphasised that this reduction in column weight significantly reduces 5 occupational health and safety (OHS) issues related to the handling of the columns.

While the wall thickness has been reduced, it is noted that the columns produced on the profiling assembly described above are capable still capable of withstanding moderate longitudinal compressive loading and also circumferential tensile loading. In many load-bearing applications, the columns do not require in-fill or additional posts. 10 Moreover, they can be erected on-site without formwork, thereby saving construction time, labour and materials.

It will be appreciated that the maximum tolerable longitudinal compressive load is dependent on the length of the column. However, indicative values for several column lengths are provided below. In terms of tensile strength, it is noted that columns of up to 15 at least 4.5m in length conform to the relevant standards required to allow for filling with wet concrete. Therefore, in applications where the columns are required to support larger compressive loads, the columns may be filled with concrete.

Columns according to the invention can also be made in a variety of shapes, including a "Classic" shape as indicated in Figure 4 and a "Tapered" shape as indicated 20 in Figure 5.

Technical information relating to column geometry and material properties is provided in the tables below by way of example only. Unless indicated to the contrary, the data relates to columns manufactured using the profiling assembly described above, on column blanks formed from FRC, using the Hatscheck process.

- 15 -

Column Type	Length (m)	Inner Diameter (mm)	Outer Diameter (mm)	Wall Thickness (mm)	Weight (kg)
Prior Art "Classic" column	2.75	176	200	12	32.7
Prior Art "Classic" column	4	176	200	12	47.6
New Lightweight "Classic" Column	2.75	176	195	9.5	25.6
New Lightweight "Classic" Column	4	176	195	9.5	37.2
Prior Art "Classic" column	2.75	233	260	13.5	47.3
Prior Art "Classic" column	4	233	260	13.5	68.8
New Lightweight "Classic" Column	2.75	233	250	8.5	32.2
New Lightweight "Classic" Column	4	233	250	8.5	46.8

OD at top of column (mm)	Column Height (mm)	B _{MIN} = 35mm				B _{MIN} = 45mm				B _{MIN} = 70mm				B _{MIN} = 90mm			
		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof	
		Sheet Roof	Tiled Roof	Sheet Roof	Tiled Roof												
195	up to 3000	166.0	101.2	144.0	96.0	101.2	144.0	160.0	112.0	160.0	112.0	101.2	144.0	160.0	101.2	101.2	144.0
	3600	157.0	102.0	137.0	93.0	157.0	139.0	174.0	125.0	157.0	139.0	152.0	139.0	174.0	125.0	177.0	139.0
(176)	4000	147.0	94.0	136.0	87.0	147.0	124.0	159.0	106.0	147.0	124.0	142.0	124.0	166.0	106.0	147.0	124.0
	up to 3000	10.3	15.3	6.5	10.3	15.3	6.5	10.3	15.3	6.5	10.3	15.3	6.5	10.3	15.3	6.5	
250	3600	8.8	13.0	5.6	8.8	13.0	5.6	8.8	13.0	5.6	8.8	13.0	5.6	8.8	13.0	5.6	
(233)	4000	7.6	11.3	4.8	7.6	11.3	4.8	7.6	11.3	4.8	7.6	11.3	4.8	7.6	11.3	4.8	
	5000	5.5	8.1	3.5	5.5	8.1	3.5	5.5	8.1	3.5	5.5	8.1	3.5	5.5	8.1	3.5	
	6000	4.1	6.1	2.6	4.1	6.1	2.6	4.1	6.1	2.6	4.1	6.1	2.6	4.1	6.1	2.6	
345	up to 4000	27.1	40.2	17.4	24.7	48.5	30.8	32.7	45.0	28.5	40.8	32.7	34.0	48.5	30.8	32.7	48.5
(304)	5000	27.1	40.2	17.4	24.7	40.6	31.4	27.4	40.6	27.4	40.6	31.4	27.4	40.6	31.4	27.4	40.6
	6000	21.3	31.6	13.5	21.3	31.6	13.5	21.3	31.6	13.5	21.3	31.6	13.5	21.3	31.6	13.5	21.3
425 (380)	up to 6000	29.6	43.9	18.8	38.2	56.6	24.2	39.0	57.7	24.7	39.0	57.7	24.7	39.0	57.7	24.7	39.0

Table 1A: Classic Architectural Columns – No Handrail Loading
Supported Roof Areas & Ultimate Loads – $E_{max} = OD/4$ (see Fig. 7)

OD at top of column (mm)	Column Height (mm)	B _{MIN} = 35mm				B _{MIN} = 45mm				B _{MIN} = 70mm				B _{MIN} = 90mm			
		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof	
		Sheet Roof	Tiled Roof	Sheet Roof	Tiled Roof												
195	up to 3000	12.5	18.5	18.0	12.5	18.5	8.0	12.5	18.5	8.0	12.5	18.5	8.0	12.5	18.5	8.0	12.5
	3600	10.7	15.0	15.0	10.7	15.8	6.8	10.7	15.8	6.8	10.7	15.8	6.8	10.7	15.8	6.8	10.7
(176)	4000	9.6	14.2	14.2	9.6	14.2	6.1	9.6	14.2	6.1	9.6	14.2	6.1	9.6	14.2	6.1	9.6
250 (233)	up to 4000	11.2	16.6	7.1	14.5	21.5	9.2	17.3	25.6	11.0	17.3	25.6	11.0	17.3	25.6	11.0	17.3
345 (304)	up to 4000	27.1	40.2	17.2	35.0	52.0	29.2	52.0	52.0	52.0	52.0	52.0	52.0	52.0	52.0	52.0	52.0

Table 1C: Tapered Architectural Columns – No Handrail Loading
Supported Roof Areas & Ultimate Loads – $E_{max} = OD/4$ (see Fig. 7)

OD at top of column (mm)	Column Height (mm)	B _{MIN} = 35mm				B _{MIN} = 45mm				B _{MIN} = 70mm				B _{MIN} = 90mm			
		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof	
		Sheet Roof	Tiled Roof	Sheet Roof	Tiled Roof												
195	up to 3000	16.9	102.6	24.4	16.9	16.9	10.2	24.4	16.9	16.9	16.9	10.2	24.4	16.9	16.9	10.2	24.4
	3600	15.7	81.5	23.6	15.7	18.5	9.3	23.6	18.5	18.5	18.5	9.3	23.6	18.5	18.5	9.3	23.6
(176)	4000	15.1	65.1	20.5	15.1	17.6	9.1	17.6	17.6	17.6	17.6	9.1	17.6	17.6	17.6	9.1	17.6
	5000	24.0	59.9	21.5	24.0	24.5	16.5	21.5	24.5	24.0	24.0	16.5	24.5	24.0	24.0	16.5	24.5
	6000	23.1	51.9	21.0	23.1	24.6	16.0	21.0	24.6	23.1	23.1	16.0	24.6	23.1	23.1	16.0	24.6
345	up to 4000	27.1	40.2	17.2	32.7	48.5	20.8	32.7	48.5	20.8	32.7	48.5	20.8	32.7	48.5	20.8	32.7
(304)	5000	25.8	38.2	18.4	25.8	38.2	16.4	25.8	38.2	16.4	25.8	38.2	16.4	25.8	38.2	16.4	25.8
	6000	20.3	30.1	12.9	20.3	30.1	12.9	20.3	30.1	12.9	20.3	30.1	12.9	20.3	30.1	12.9	20.3
425 (380)	up to 6000	29.6	43.9	18.8	37.5	55.5	23.8	37.5	55.5	23.8	37.5	55.5	23.8	37.5	55.5	23.8	37.5

Table 1D: Classic Architectural Columns – Handrail Loading
Supported Roof Areas & Ultimate Loads – $E_{max} = OD/4$ (see Fig. 7)

OD at top of column (mm)	Column Height (mm)	B _{MIN} = 35mm				B _{MIN} = 45mm				B _{MIN} = 70mm				B _{MIN} = 90mm			
		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof		Ult Load (kN)		Supported Roof	
		Sheet Roof	Tiled Roof	Sheet Roof	Tiled Roof												
195	up to 3000	15.0	74.0	31.0	15.0	50.0	27.7	45.0	31.0	50.0	27.7	45.0	31.0	50.0	27.7	45.0	31.0
	3600	14.5	65.5	28.0	14.5	44.2	24.5	41.5	28.0	44.2	24.5	41.5	28.0	44.2	24.5	41.5	28.0
(176)	4000	14.0	59.5	25.5	14.0	35.0	21.5	35.0	25.5	40.0	21.5	35.0	25.5	40.0	21.5	35.0	25.5
250 (233)	up to 4000	8.2	12.1	5.2	8.2	12.1	5.2	8.2	12.1	5.2	8.2	12.1	5.2	8.2	12.1	5.2	8.2
345 (304)	up to 4000	27.1	40.2	17.2	35.0	51.9	22.9	47.4	35.0	51.9	22.9	47.4	35.0	51.9	22.9	47.4	35.0

Table 1F: Tapered Architectural Columns – Handrail Loading
Supported Roof Areas & Ultimate Loads – $E_{max} = OD/4$ (see Fig. 7)

of column (mm)	Column Height (mm)	$E_{MAX}=OD/3$					$E_{MAX}=OD/2+50\text{mm}$				
		One N16	Three N12	Three N16	Four N12	Four N16	One N16	Three N12	Three N16	Four N12	Four N16
		105	125	115	139	23	137	153	150	164	164
250 (233)	up to 900	168	105	125	115	139	23	137	153	150	164
	1800	193	152	182	175	196	30	142	166	163	179
	195	200	133	136	165	171	79	143	168	165	181
	2400	181	136	136	161	171	79	143	168	165	181
	3000	187	127	152	148	165	55	151	172	170	189
	3600	175	120	140	139	154	50	121	142	142	154
345 (304)	up to 1800	166	103	128	119	134	25	134	157	152	177
	2400	191	128	191	191	209	47	62	195	190	142
	3000	188	110	167	168	199	42	58	180	184	135
	3600	175	109	152	148	176	38	54	185	178	126
	4000	167	86	134	136	174	35	50	179	174	123
	425 (380)	up to 1800	232	281	362	354	439	77	103	144	134
425 (380)	2400	177	209	274	277	384	68	92	131	121	190
	3000	156	185	248	249	359	63	87	125	115	183
	4000	126	152	207	207	316	56	79	114	104	169

Table 2A: Ultimate Axial Compression Capacities (kN) for Pinned Base Footing (see Fig. 8)

of column (mm)	Column Height (mm)	$E_{MAX}=OD/3$					$E_{MAX}=OD/2+50\text{mm}$				
		One N16	Three N12	Three N16	Four N12	Four N16	One N16	Three N12	Three N16	Four N12	Four N16
		105	125	115	139	23	137	153	150	164	164
250 (233)	up to 900	166	105	125	115	139	23	137	153	150	164
	1800	190	152	191	184	196	30	133	159	156	173
	195	200	145	174	169	190	29	141	163	160	177
	2400	181	136	145	141	165	29	141	163	160	177
	3000	187	127	152	148	176	29	146	170	167	182
	3600	175	120	150	147	164	25	141	162	159	178
345 (304)	up to 1800	166	103	128	119	134	25	134	157	152	177
	2400	191	128	191	191	209	47	62	195	190	142
	3000	188	110	167	168	199	42	58	180	184	135
	3600	175	109	152	148	176	38	54	185	178	126
	4000	167	86	134	136	174	35	50	179	174	123
	425 (380)	up to 1800	74	112	166	155	195	34	45	75	73
345 (304)	2400	59	88	140	136	177	29	39	69	67	94
	3000	48	71	119	120	160	25	35	63	61	89
	3600	40	59	104	105	143	22	31	58	57	83
	4000	35	52	95	96	133	20	29	55	54	79
425 (380)	up to 3000	172	202	269	269	378	67	91	130	119	188
	4000	143	171	231	232	342	60	84	120	111	177

Table 2B: Ultimate Axial Compression Capacities (kN) for Fixed Base Footing (see Fig. 9)

- 18 -

Fixing	Grade	Min. Fixing Lap/Embe	Ultimate Uplift Force Per
M10	Grade 250	250	12
	4.6/S	250	18
	8.8/S	400	40
	Grade 250	300	17
	4.6/S	300	27
	8.8/S	550	58
M12	Grade 250	400	31
	4.6/S	450	50
	8.8/S	900	104
	N12	500MPa	350
	N16	500MPa	550
	N16	500MPa	900

Table 3: Uplift Capacity (kN)

OD at top of column (mm)	Column Height (mm)	One	One	One N12	One N16	Three N12	Three N16	Four N12	Four N16
		M12	M16			4.6/S MIN	4.6/S MIN		
195 (176)	600	13.0	14.7	3.5	5.0	8.0	10.5	11.5	19.3
	900	21.0	23.1	5.3	7.0	11.7	12.9	13.7	34.2
	1200	21.0	23.1	5.3	7.0	11.7	12.9	13.7	34.2
	1500	21.0	23.1	5.3	7.0	11.7	12.9	13.7	34.2
	1800	21.0	23.1	5.3	7.0	11.7	12.9	13.7	34.2
	2100	21.0	23.1	5.3	7.0	11.7	12.9	13.7	34.2
	2400	21.0	23.1	5.3	7.0	11.7	12.9	13.7	34.2
250 (233)	3000	16.2	19.0	7.0	10.0	16.6	21.1	22.9	39.9
	3600	15.1	19.6	6.6	9.8	13.7	18.1	19.9	35.2
	4000	10.5	10.7	5.5	10.8	12.2	16.1	17.7	29.5
	600	5.0	8.5	6.0	10.0	13.2	25.0	20.8	35.0
	900	3.3	5.7	4.0	6.7	8.8	16.7	13.9	23.3
	1800	1.7	2.8	2.0	3.3	4.4	8.3	6.9	11.7
345 (304)	2400	1.3	2.1	1.5	2.5	3.3	6.3	5.2	8.8
	3000	1.0	1.7	1.2	2.0	2.6	5.0	4.2	7.0
	3600	0.8	1.4	1.0	1.7	2.2	4.2	3.5	5.8
	4000	0.8	1.3	0.9	1.5	2.0	3.8	3.1	5.3
	600	7.3	12.7	8.8	15.5	23.3	37.7	31.0	62.2
	900	4.9	8.4	5.9	10.3	15.6	25.1	20.7	34.8
425 (380)	1200	2.4	4.2	2.9	5.2	7.8	12.6	10.3	17.4
	1800	1.8	3.2	2.2	3.9	5.8	9.4	7.8	13.0
	2400	1.5	2.5	1.8	3.1	4.7	7.5	6.2	10.4
	3000	1.2	2.1	1.5	2.6	3.9	6.3	6.2	8.7
	3600	1.1	1.9	1.3	2.3	3.5	5.7	4.7	7.8
	4000	1.5	2.5	1.8	3.1	5.2	8.1	6.4	10.6

Table 4: Ultimate Horizontal Capacity (kN) for Fixed Base Footing Only (see Fig. 9)

It will be appreciated that the illustrated profiling assembly can be used to profile columns having diameters other than those listed in the tables above. It will also be appreciated that the assembly is particularly useful for profiling lightweight FRC columns, as the provision of multiple lateral supports adjacent the position of the 5 profiling tool minimises vibration during profiling. This in turn prevents fracture of the columns near the chucks and also improves the quality of the profiled surface in the finished product. The applicant has also found that the illustrated profiling assembly improves the finished quality of the profiled surface in heavier FRC columns. The 10 columns formed on the profiling assembly have a surface finish conducive to a receiving any one of a variety of coatings, such as paint, render, textured finishes and tiles. In all these respects, the invention represents a practical and commercially significant improvement over the prior art.

Architectural columns produced using the above-described method are suited for use in a variety of applications. For example, they can be placed over electrical or 15 plumbing services to hide the services and thereby enhance the aesthetic properties of a building by giving the impression of a solid marble or concrete column. In addition, the columns can be used in a variety of other load-bearing and non-load-bearing applications.

It will be appreciated by those skilled in the art that while the invention has been 20 described with reference to specific examples, it may also be embodied in many other forms.

CLAIMS

1. A fibre reinforced cement tubular body having a wall thickness to outer diameter ratio of less than around 0.050.
2. A fibre reinforced cement tubular body according to claim 1 wherein the body has
5 a wall thickness to outer diameter ratio of less than around 0.045.
3. A fibre reinforced cement tubular body according to claim 2 wherein the body has
a wall thickness to outer diameter ratio of less than around 0.035.
4. A fibre reinforced cement tubular body according to any one of the preceding
claims wherein an outer circumferential surface of the body is machined or profiled to
10 achieve the wall thickness to outer diameter ratio.
5. A fibre reinforced cement tubular body according to claim 4 wherein the body is
machined or profiled on a lathe assembly.
6. A fibre reinforced cement tubular body according to claim 5 wherein the body is
formed from a fibre reinforced cement blank manufactured on a mandrel using a
15 Hatschek process.
7. A fibre reinforced cement tubular body according to claim 6 wherein an initial
wall thickness of the blank is substantially reduced and a surface finish of the blank is
refined to form the body.
8. A fibre reinforced cement tubular body according to any one of the preceding
20 claims adapted for use as an architectural column.
9. A fibre reinforced cement tubular body according to any one of claims 1 to 7
adapted for use as a pipe, structural member or concrete forming element.
10. A lathe assembly for forming an elongate tubular body, said lathe assembly
including:
25 an elongate base;
 a pair of chucks located at opposite longitudinal ends of said base, said chucks
being configured to engage opposite longitudinal ends of the tubular body;

- two or more lateral supports connected to said base to support the tubular body at two or more support locations between its ends;
- drive means for rotating the body about a longitudinal axis; and
- a profiling tool connected to the base and engageable to machine or profile an outer circumferential surface of the tubular body.
11. A lathe assembly according to claim 10 wherein two or more of the lateral support locations are located at substantially the same axial position along the length of the body.
12. A lathe assembly according to claim 10 or claim 11 wherein two or more of the lateral support locations are located at different axial positions along the body.
13. A lathe assembly according to claim 11 or claim 12 wherein two or more of the lateral support locations are spaced circumferentially around the body.
14. A lathe assembly according to any one of claims 10 to 13 wherein the lateral supports take the form of support rollers engageable with an outer circumferential surface of the body.
15. A lathe assembly according to claim 14 wherein the support rollers and the profiling tool are adapted to move in unison along the length of the body, so as to remain in their relative axial locations during the profiling operation.
16. A lathe assembly according to claim 14 adapted to move the elongate body longitudinally in relation to the support rollers and the profiling tool, such that the support rollers and the profiling tool remain in their relative axial locations during the profiling operation.
17. A lathe assembly according to any one of claims 14 to 16 wherein two of the support rollers are dependently movable into engagement with the body.
- 25 18. A lathe assembly according to claim 17 wherein the dependently movable support rollers are hingedly mounted to opposite ends of a first bell crank lever having an axis of rotation substantially parallel to the longitudinal axis of the body.

- 22 -

19. A lathe assembly according to claim 18 wherein the first bell crank lever is hingedly connected to one end of a second bell crank lever having an axis of rotation substantially parallel to the longitudinal axis of the body.
20. A lathe assembly according to claim 19 wherein the other end of the second bell
5 crank lever is rotatably connected to a first base plate.
21. A lathe assembly according to claim 20 wherein the first base plate is longitudinally movable along the elongate base.
22. A lathe assembly according to claim 20 or claim 21 wherein the first base plate is selectively fixedly connectable to the elongate base in any one of a plurality of axial
10 locations.
23. A lathe assembly according to any one of claims 19 to 22 wherein a pneumatic actuator is operable on the second bell crank lever to move the respective rollers into and out of engagement with the body.
24. A lathe assembly according to any one of claims 14 to 23 wherein two of the
15 support rollers are independently movable into engagement with the body.
25. A lathe assembly according to claim 24 wherein the independently movable support roller is mounted to one end of a hingeable arm.
26. A lathe assembly according to claim 25 wherein the arm has an axis of rotation substantially parallel to the longitudinal axis of the body.
- 20 27. A lathe assembly according to claim 25 or claim 26 wherein the other end of the arm is hingedly connected to a second base plate.
28. A lathe assembly according to claim 27 wherein the second base plate is longitudinally movable along the elongate base.
29. A lathe assembly according to claim 27 or claim 28 wherein the second base plate
25 is selectively fixedly connectable to the elongate base in any one of a plurality of axial locations.

- 23 -

30. A lathe assembly according to any one of claims 25 to 29 wherein a pneumatic actuator is operable on the arm to move the respective roller into and out of engagement with the body.
31. A lathe assembly according to any one of claims 14 to 30 including three of the support rollers, two of the support rollers being movable into engagement with the body independently of the third support roller.
32. A lathe assembly according any one of claims 14 to 31 wherein at least one of the support rollers is radially movable in response to imperfections in the outer circumferential surface of the body.
- 10 33. A lathe assembly according to any one of claims 10 to 32 wherein the profiling tool when in use is located axially adjacent one of the lateral support locations.
34. A lathe assembly according to any one of claims 10 to 33 wherein the profiling tool is longitudinally movable along the elongate base.
- 15 35. A lathe assembly according to any one of claims 10 to 34 wherein the profiling tool is selectively fixedly connectable to the elongate base in any one of a plurality of axial locations.
36. A lathe assembly according to any one of claims 10 to 35 wherein the body is formed of fibre reinforced cement.
- 20 37. A lathe assembly according to claim 36 wherein the body is formed from a fibre reinforced cement blank manufactured on a mandrel using a Hatschek process.
38. A lathe assembly according to claim 37 used to substantially reduce the initial wall thickness and refine the surface finish of the blank to form the body.
39. A lathe assembly according to any one of claims 10 to 38 wherein the body has a wall thickness to outer diameter ratio of less than around 0.050.
- 25 40. A lathe assembly according to claim 39 wherein the body has a wall thickness to outer diameter ratio of less than around 0.045.
41. A lathe assembly according to claim 40 wherein the body has a wall thickness to outer diameter ratio of less than around 0.035.

- 24 -

42. A lathe assembly according to any one of claims 10 to 41 wherein the body is an architectural column.
43. A lathe assembly according to any one of claims 10 to 41 wherein the body is a pipe, a structural member or a concrete forming element.
- 5 44. An elongate tubular body formed on a lathe assembly according to any one of claims 10 to 43.
45. An elongate tubular body formed of fibre reinforced cement on a lathe assembly according to any one of claims 10 to 43.
- 10 46. An elongate tubular body formed from a fibre reinforced cement blank on a lathe assembly according to any one of claims 10 to 43, wherein the blank is manufactured on a mandrel using a Hatschek process.
47. An elongate tubular body according to claim 46 wherein the lathe assembly is used to substantially reduce the initial wall thickness and refine the surface finish of the blank to form the body.
- 15 48. An elongate tubular body according to any one of claims 45 to 47 having a wall thickness to outer diameter ratio of less than around 0.050.
49. An elongate tubular body according to claim 48 having a wall thickness to outer diameter ratio of less than around 0.045.
50. An elongate tubular body according to claim 49 having a wall thickness to outer diameter ratio of less than around 0.035.
- 20 51. An elongate tubular body according to any one of claims 44 to 50 adapted for use as an architectural column.
52. An elongate tubular body according to any one of claims 44 to 50 adapted for use as a pipe, structural member or concrete forming element.
- 25 53. A method of manufacturing an elongate tubular body, said method including the steps of:
supporting the body at or adjacent its ends for rotation about a longitudinal axis;

supporting the body laterally at two or more lateral support locations between the ends;

rotating the body about the longitudinal axis; and

machining or profiling an outer surface of the body using a profiling tool.

- 5 54. A method according to claim 53 wherein two or more of the lateral support locations are located at substantially the same axial position along the length of the body.
55. A method according to claim 53 or claim 54 wherein two or more of the support locations are located at different axial positions along the body.
- 10 56. A method according to claim 54 or claim 55 wherein two or more of the lateral support locations are spaced circumferentially around the body.
57. A method according to any one of claims 53 to 56 wherein the lateral support is provided by respective support rollers engageable with an outer circumferential surface of the body.
- 15 58. A method according to claim 57 wherein the support rollers and the profiling tool are moved in unison along the length of the body, so as to remain in their relative axial locations during the profiling operation.
59. A method according to claim 57 wherein the elongate body is moved longitudinally in relation to the support rollers and the profiling tool, such that the support rollers and the profiling tool remain in their relative axial locations during the profiling operation.
- 20 60. A method according to any one of claims 57 to 59 wherein two of the support rollers are dependently moved into engagement with the body.
61. A method according to claim 60 wherein the dependently movable support rollers are hingedly mounted to opposite ends of a first bell crank lever having an axis of rotation substantially parallel to the longitudinal axis of the body.
- 25 62. A method according to claim 61 wherein the first bell crank lever is hingedly connected to one end of a second bell crank lever having an axis of rotation parallel to the longitudinal axis of the body.

- 26 -

63. A method according to claim 62 wherein the other end of the second bell crank lever is rotatably connected to a first base plate.
64. A method according to claim 63 wherein the first base plate is longitudinally moved along the elongate base.
- 5 65. A method according to claim 63 or claim 64 wherein the first base plate is selectively fixedly connected to the elongate base in any one of a plurality of axial locations.
66. A method according to any one of claims 62 to 65 wherein a pneumatic actuator is operatively applied to the second bell crank lever to move the respective rollers into and 10 out of engagement with the body.
67. A method according to any one of claims 57 to 66 wherein two of the support rollers are independently moved into engagement with the body.
68. A method according to claim 67 wherein the independently moved support roller is mounted to one end of a hingeable arm.
- 15 69. A method according to claim 68 wherein the arm has an axis of rotation parallel to the longitudinal axis of the body.
70. A method according to claim 68 or claim 69 wherein the other end of the arm is hingedly connected to a second base plate.
71. A method according to claim 70 wherein the second base plate is longitudinally 20 moved along the elongate base.
72. A method according to claim 70 or claim 71 wherein the second base plate is selectively fixedly connected to the elongate base in any one of a plurality of axial locations.
73. A method according to any one of claims 68 to 72 wherein a pneumatic actuator is 25 operatively applied on the arm to move the respective roller into and out of engagement with the body.

- 27 -

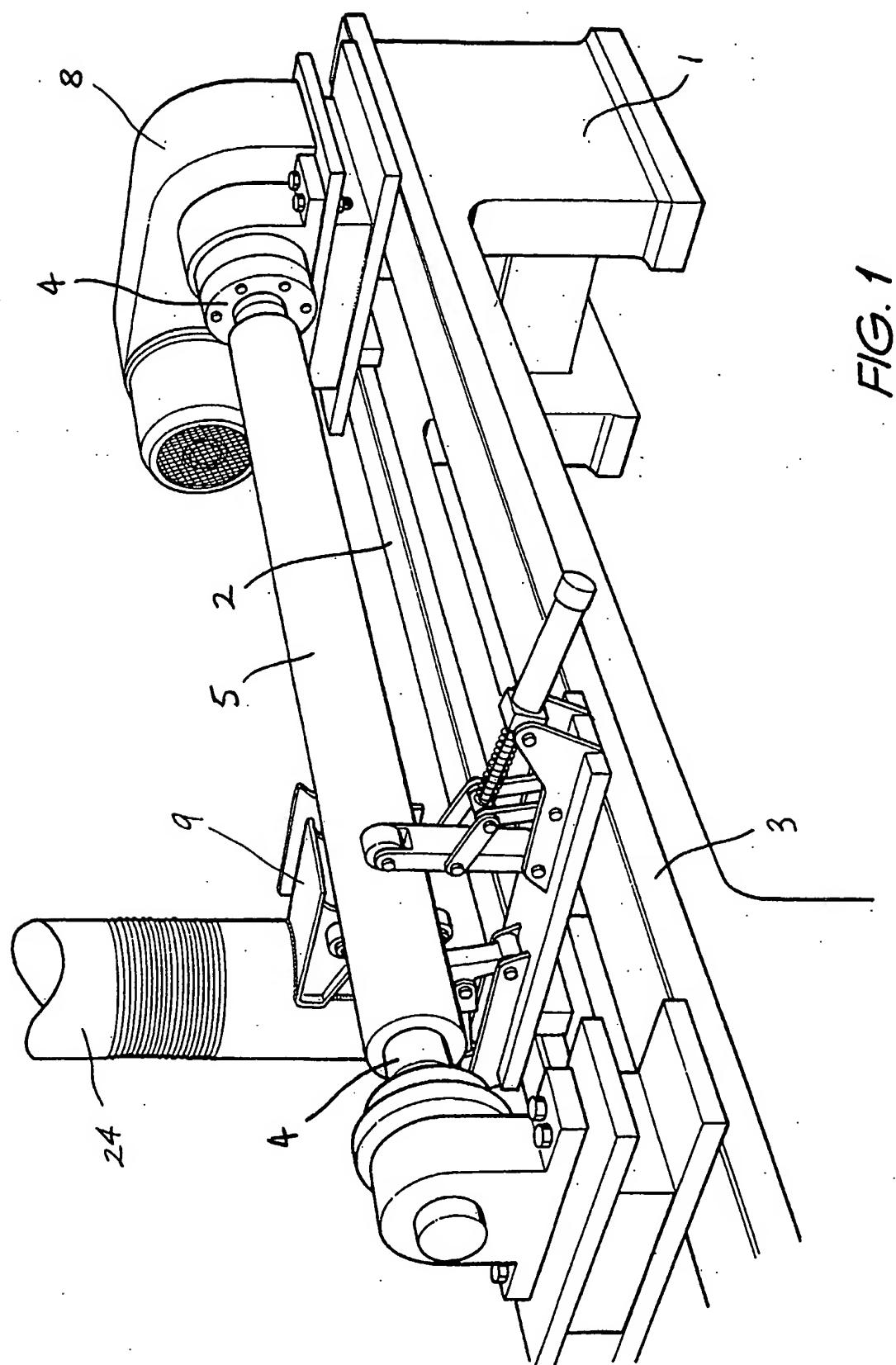
74. A method according to any one of claims 57 to 73 wherein three of the support rollers are provided, two of the support rollers being movable into engagement with the body independently of the third support roller.
75. A method according any one of claims 57 to 74 wherein at least one of the support rollers is configured to move radially in response to imperfections in the outer circumferential surface of the body.
5
76. A method according to any one of claims 53 to 75 wherein the profiling tool when in use is located axially adjacent one of the lateral support locations.
77. A method according to any one of claims 53 to 76 wherein the profiling tool is longitudinally moved along the elongate base.
10
78. A method according to any one of claims 53 to 77 wherein the profiling tool is selectively fixedly connected to the elongate base in any one of a plurality of axial locations.
79. A method according to any one of claims 53 to 78 wherein the body is formed of fibre reinforced cement.
15
80. A method according to claim 79 wherein the body is formed from a fibre reinforced cement blank manufactured on a mandrel using a Hatschek process.
81. A method according to claim 80 including the steps of substantially reducing the initial wall thickness and refining the surface finish of the blank to form the body.
20
82. A method according to any one of claims 53 to 81 wherein the body is machined or profiled to a wall thickness to outer diameter ratio of less than around 0.050.
83. A method according to claim 82 wherein the body is machined or profiled to a wall thickness to outer diameter ratio of less than around 0.045.
84. A method according to claim 83 wherein the body is machined or profiled to a wall thickness to outer diameter ratio of less than around 0.035.
25
85. A method according to any one of claims 53 to 84 wherein the body is machined or profiled on a lathe assembly.

- 28 -

86. A method according to any one of claims 53 to 85 wherein the body is an architectural column.
87. A method according to any one of claims 53 to 85 wherein the body is a pipe, a structural member or a concrete forming element.
- 5 88. An elongate tubular body manufactured by the method according to any one of claims 53 to 87.
89. An elongate tubular body manufactured on a lathe assembly by the method according to any one of claims 53 to 87.
90. An elongate tubular body formed of fibre reinforced cement by the method
10 according to any one of claims 53 to 87.
91. An elongate tubular body formed from a fibre reinforced cement blank by the method according to any one of claims 53 to 87, wherein the blank is manufactured on a mandrel using a Hatschek process.
92. An elongate tubular body according to claim 91 wherein the method includes the
15 steps of substantially reducing the initial wall thickness and refining the surface finish of the blank to form the body.
93. An elongate tubular body according to any one of claim 90 to 92 having a wall thickness to outer diameter ratio of less than around 0.050.
94. An elongate tubular body according to claim 93 having a wall thickness to outer
20 diameter ratio of less than around 0.045.
95. An elongate tubular body according to claim 94 having a wall thickness to outer diameter ratio of less than around 0.035.
96. An elongate tubular body according to any one of claims 88 to 95 adapted for use as an architectural column.
- 25 97. An elongate tubular body according to any one of claims 88 to 95 adapted for use as a pipe, structural member or concrete forming element.

- 29 -

98. A fibre reinforced cement tubular body substantially as herein described with reference to any one of the embodiments of the invention illustrated in the accompanying drawings and/or examples.
99. An elongate tubular body substantially as herein described with reference to any 5 one of the embodiments of the invention illustrated in the accompanying drawings and/or examples.
100. A lathe assembly substantially as herein described with reference to any one of the embodiments of the invention illustrated in the accompanying drawings and/or examples.
101. A method of manufacturing an elongate tubular body substantially as herein described with reference to any one of the embodiments of the invention illustrated in the accompanying drawings and/or examples.



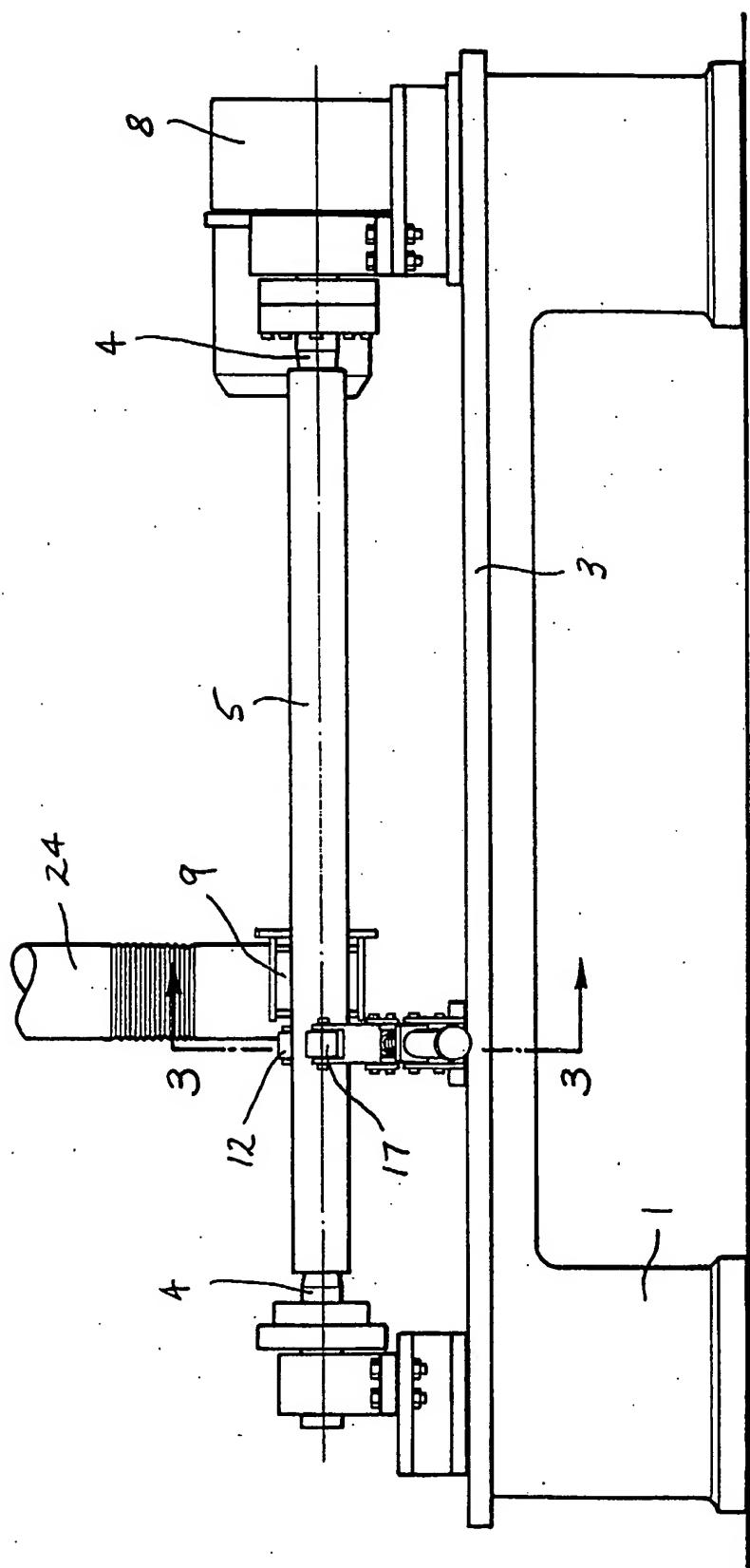


FIG. 2

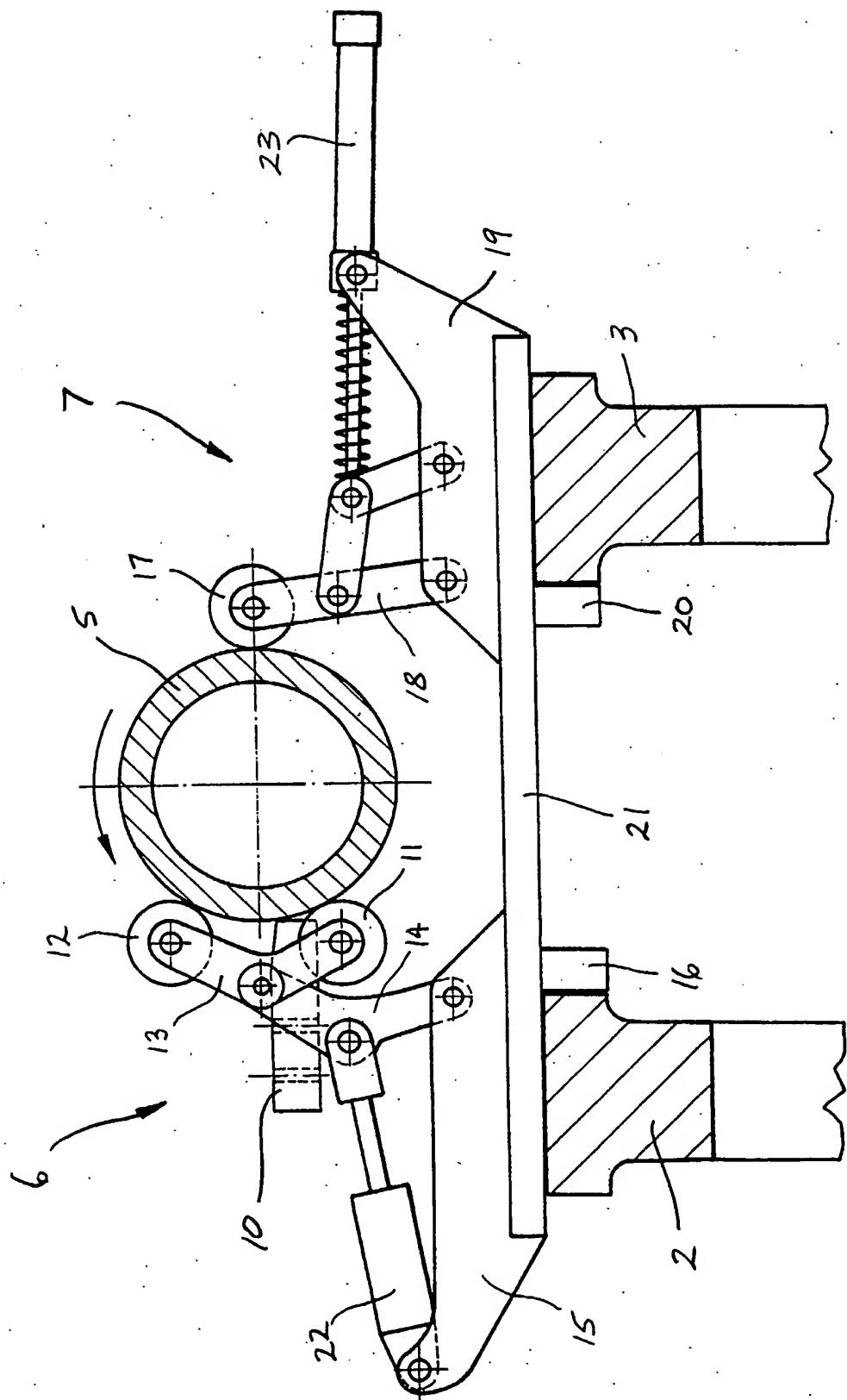
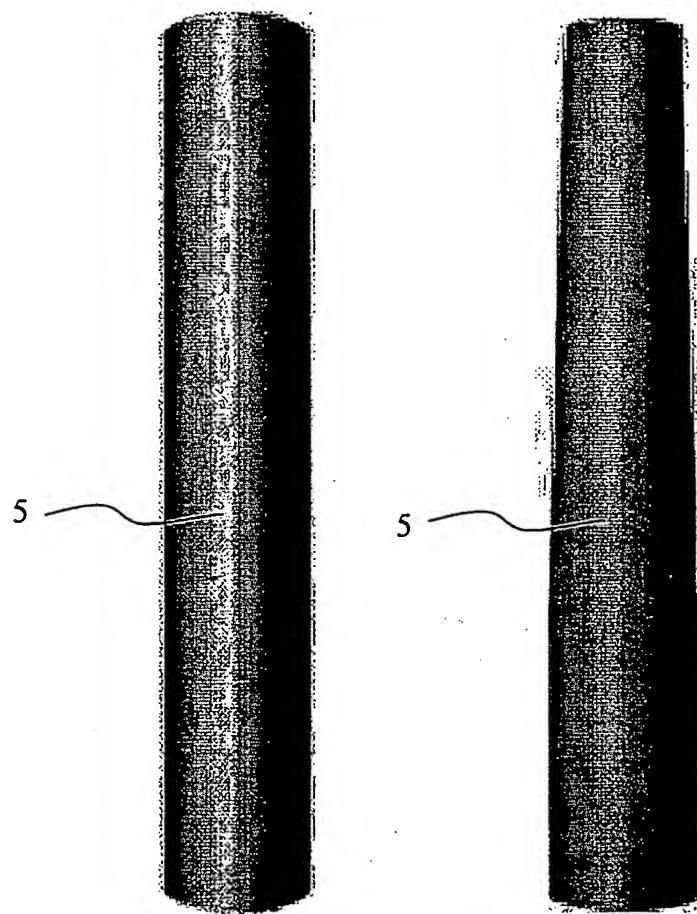
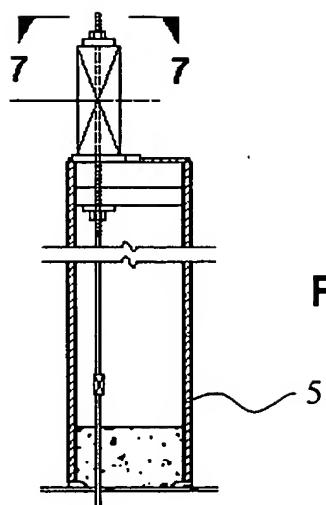
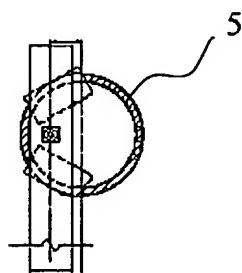
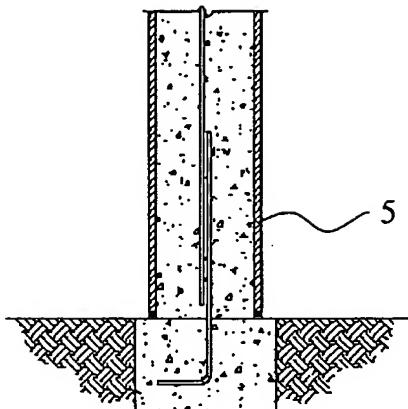
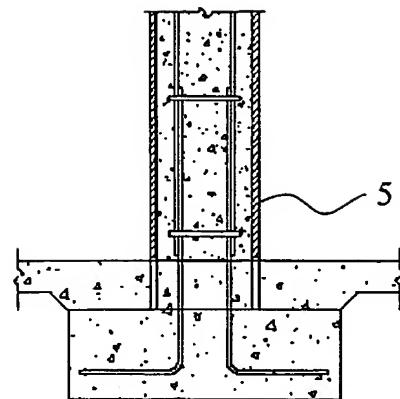
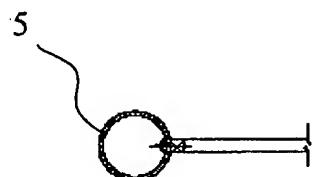
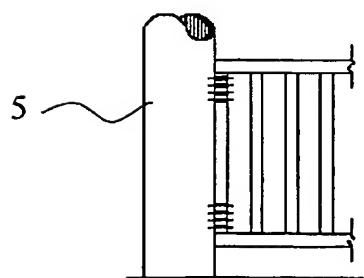


FIG. 3

**FIGURE 4****FIGURE 5**

**FIGURE 6****FIGURE 7**

**FIGURE 8****FIGURE 9****FIGURE 10****FIGURE 11**

INTERNATIONAL SEARCH REPORT

International application No.
PCT/AU2004/001378

A. CLASSIFICATION OF SUBJECT MATTER		
Int. Cl. ⁷ : B28B 21/92, 21/96, E04C 3/34		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols)		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) DWPI IPC B28B 21/92, 21/96, E04C 3/34, B28D 1/16, B23B/IC and Keywords; USPTO and Keywords; esp@cenet Database and Keywords		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0633107 B (PT-POLY-TEC GMBH) 11 January 1995 See figures 1-4	10-14, 16-17, 34-38, 42-47, 51-57, 59-60, 77-81, 85-92, 96-97
X	EP 566879 A (WENSAUER BETONWERK GMBH) 27 October 1993 See whole document	10-14, 16-17, 34-38, 42-47, 51-57, 59-60, 77-81, 85-92, 96-97
X	US 5595524 A (GUNDY) 21 January 1997 See figures 1-3	10-14, 16-17, 34-38, 42-47, 51-57, 59-60, 77-81, 85-92, 96-97
X	US 3985848 A (FRISCHE ET AL.) 12 October 1976 See whole document	10-14, 16-17, 34-38, 42-47, 51-57, 59-60, 77-81, 85-92, 96-97
<input type="checkbox"/> Further documents are listed in the continuation of Box C <input checked="" type="checkbox"/> See patent family annex		
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed		
Date of the actual completion of the international search 28 October 2004	Date of mailing of the international search report 5 NOV 2004	
Name and mailing address of the ISA/AU AUSTRALIAN PATENT OFFICE PO BOX 200, WODEN ACT 2606, AUSTRALIA E-mail address: pct@ipaaustralia.gov.au Facsimile No. (02) 6285 3929	Authorized officer JOHN DEUIS Telephone No : (02) 6283 2146	

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/AU2004/001378

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Report		Patent Family Member	
EP	0633107	DE	4025603
EP	0566879		EP 0471319
US	5595524	WO	9625271
US	3985848	GB	1504051
		GB	1504052
		NL	7502800

Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001.

END OF ANNEX

**This Page is Inserted by IFW Indexing and Scanning
Operations and is not part of the Official Record**

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- BLACK BORDERS**
- IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- FADED TEXT OR DRAWING**
- BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- SKEWED/SLANTED IMAGES**
- COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- GRAY SCALE DOCUMENTS**
- LINES OR MARKS ON ORIGINAL DOCUMENT**
- REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- OTHER:** _____

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.